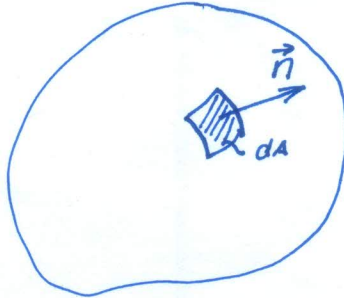
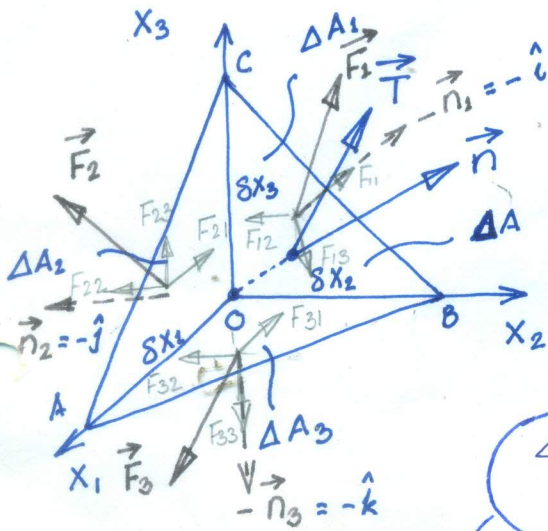


ALL ABOUT STRESS!



$$\Delta A_1 = \frac{1}{2} \delta X_2 \cdot \delta X_3; \quad \Delta A_2 = \frac{1}{2} \delta X_1 \cdot \delta X_3;$$

$$\Delta A_3 = \frac{1}{2} \delta X_1 \cdot \delta X_2$$

$$\Delta A \vec{n} = \Delta A = \frac{1}{2} (\vec{AB} \times \vec{AC})$$

$$= \frac{1}{2} (-\delta X_1 \hat{i} + \delta X_2 \hat{j}) \times (-\delta X_1 \hat{i} + \delta X_3 \hat{k})$$

$$= \Delta A_1 \hat{i} + \Delta A_2 \hat{j} + \Delta A_3 \hat{k}$$

Now  $\Delta A_1 = \Delta A \cdot n_1$ ;  $\Delta A_2 = \Delta A \cdot n_2$ ;  $\Delta A_3 = \Delta A \cdot n_3$

where  $\vec{n} = n_1 \hat{i} + n_2 \hat{j} + n_3 \hat{k}$

∴ force balance:

Lt  $\delta X_i \rightarrow 0$

$$\vec{T} \Delta A + \vec{F}_1 \frac{\Delta A_1}{\Delta A n_1} + \vec{F}_2 \frac{\Delta A_2}{\Delta A n_2} + \vec{F}_3 \frac{\Delta A_3}{\Delta A n_3} + \frac{\Delta V \cdot \vec{f}}{\Delta A} = 0$$

$$\Rightarrow \vec{T} = -(\vec{F}_1 n_1 + \vec{F}_2 n_2 + \vec{F}_3 n_3)$$

$$= -F_{11} \hat{i} - F_{12} \hat{j} - F_{13} \hat{k} - F_{21} \hat{i} - F_{22} \hat{j} - F_{23} \hat{k} - F_{31} \hat{i} - F_{32} \hat{j} - F_{33} \hat{k}$$

$$= (F_{11} n_1 + F_{21} n_2 + F_{31} n_3) \hat{i} + (F_{12} n_1 + F_{22} n_2 + F_{32} n_3) \hat{j}$$

$$+ (F_{13} n_1 + F_{23} n_2 + F_{33} n_3) \hat{k}$$

$$= T_1 \hat{i} + T_2 \hat{j} + T_3 \hat{k}$$

$$\therefore \boxed{T_i = F_{ji} n_j}$$

↑  
stress (force per unit area)

$$= \underbrace{\sigma_{ji} n_j}_{\text{Cauchy Stress}} = [\sigma]^T \{n\}$$

Cauchy's hypothesis: The local, pointwise traction vector  $\vec{T}$  is a linear function of the normal vector  $\vec{n}$ .  $[\sigma]$  is the operator and is called the stress tensor.

This relationship is true for any PORTION P of B, i.e.

$$\vec{T}|_{\partial P} = [\sigma]^T \vec{n}|_{\partial P}$$

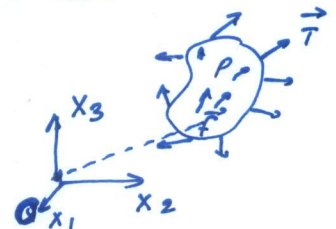
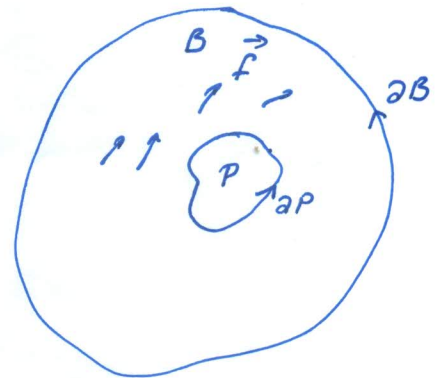
Now the portion also has to be in equilibrium or

$$\int_P \vec{f} dV + \int_{\partial P} \vec{T} dA = \vec{0}$$

$$\Rightarrow \int_P \vec{f} dV + \int_{\partial P} [\sigma]^T \vec{n} dA = \vec{0}$$

$$\Downarrow \int_P f_i dV + \int_{\partial P} \sigma_{ji} n_j dA = 0 \quad ; i=1,2,3$$

$$\Rightarrow \int_P (f_i + \sigma_{ji,j}) dV = 0 \quad \leftarrow \text{true for all arbitrary portions} \Rightarrow \boxed{f_i + \sigma_{ji,j} = 0}$$



Moment balance:

Take moment about origin

$$\Rightarrow \int_P \underbrace{\vec{r} \times \vec{f}}_{r_i f_j \vec{e}_k} dV + \int_{\partial P} \underbrace{\vec{r} \times \vec{T}}_{r_i T_j \vec{e}_k} dA = \vec{0}$$

Force balance equation

(i,j,k in cyclic symmetry)

Let us look at a specific case:

$$\int_P r_2 f_2 \vec{e}_3 dv + \int_{\partial P} r_2 \underbrace{T_2}_{(\sigma_{12} n_1 + \sigma_{22} n_2 + \sigma_{32} n_3)} \vec{e}_3 dA$$

$$\int_P (\underbrace{r_2}_{x_1} \sigma_{12})_{,1} + (\underbrace{r_2}_{x_1} \sigma_{22})_{,2} + (\underbrace{r_2}_{x_1} \sigma_{32})_{,3}$$

$$\int_P (\sigma_{12} + x_1 \sigma_{12,1} + x_1 \sigma_{22,2} + x_1 \sigma_{32,3}) dv$$

$$\int_P (\sigma_{12} + x_1 (-f_2)) dv + \int_P x_1 f_2 dv = \int_P \sigma_{12} dv$$

Similarly,

$$\int_P -r_2 f_1 \vec{e}_3 dv + \int_{\partial P} -r_2 \underbrace{T_2}_{(\sigma_{11} n_1 + \sigma_{21} n_2 + \sigma_{31} n_3)} \vec{e}_3 dA$$

$$= \int_P -x_2 f_1 \vec{e}_3 - \int_P \{ (\sigma_{11} x_2)_{,1} + (\sigma_{21} x_2)_{,2} + (\sigma_{31} x_2)_{,3} \} dv$$

$$- \int_P x_2 (\underbrace{\sigma_{11,1} + \sigma_{21,2} + \sigma_{31,3}}_{-f_1}) dv - \int_P \sigma_{21} dv = \int_P -\sigma_{21} dv$$

⇒ Corresponding to  $\vec{e}_3$ , we have  $\int_P (\sigma_{12} - \sigma_{21}) dv = 0$

⇒  $\sigma_{12} = \sigma_{21}$  ← Stress symmetry!

OR  $\sigma_{ij} = \sigma_{ji} \Rightarrow [\sigma]^T = [\sigma]$

This means that stress tensor is symmetric ⇒

when we look for those specific directions  $\vec{n}$  such that

$$\vec{T} = [\sigma] \vec{n} = \lambda \vec{n} \sim \text{i.e. } \vec{T} \text{ directed along } \vec{n}$$

⇒  $\lambda_i \rightarrow$  EIGENVALUE,  $\vec{n}^{(i)} \rightarrow$  EIGENVECTOR

3 perpendicular directions ~ PRINCIPAL DIRECTIONS

