

Consequences of strain derivation



Let $\vec{PQ}_i = \vec{\Delta X}^{(i)}$ and $\vec{P'Q}'_i = \vec{\Delta X}'^{(i)}$, then
 with $l_0^{(i)} = |\vec{\Delta X}^{(i)}|$; $l^{(i)} = |\vec{\Delta X}'^{(i)}|$, we have

$$\frac{\Delta l^{(i)}}{l_0^{(i)}} = \frac{l^{(i)} - l_0^{(i)}}{l_0^{(i)}} = \frac{\vec{\Delta X}^{(i)T} [\epsilon] \vec{\Delta X}^{(i)}}{l_0^{(i)2}}$$

where $[\epsilon] \Big|_P = \begin{bmatrix} \epsilon_{11} & \epsilon_{12} & \epsilon_{13} \\ \epsilon_{12} & \epsilon_{22} & \epsilon_{23} \\ \epsilon_{13} & \epsilon_{23} & \epsilon_{33} \end{bmatrix}_{\text{at } P}$ as the strain tensor at \underline{P} .

- Knowing $[\epsilon] \Big|_P$ we can get stretch of ANY infinitesimal line element \vec{PQ}_i at P .

E.g. $\vec{\Delta X}^{(1)} = \Delta x \hat{i} \Rightarrow \frac{\Delta l^{(1)}}{l_0^{(1)}} = \frac{\{\Delta x \ 0 \ 0\} \begin{Bmatrix} \epsilon_{11} \Delta x \\ \epsilon_{21} \Delta x \\ \epsilon_{31} \Delta x \end{Bmatrix}}{\Delta x^2}$

$= \frac{\epsilon_{11} \cdot \Delta x^2}{\Delta x^2} = \epsilon_{11}$

$\vec{\Delta X}^{(2)} = \frac{\Delta x}{\sqrt{2}} (\hat{i} + \hat{j}) \Rightarrow \frac{\Delta l^{(2)}}{l_0^{(2)}} = \frac{\Delta x^2 \{1 \ 1 \ 0\} \begin{Bmatrix} \epsilon_{11} + \epsilon_{12} \\ \epsilon_{21} + \epsilon_{22} \\ \epsilon_{31} + \epsilon_{32} \end{Bmatrix} \times \frac{1}{2}}{\Delta x^2}$

$= \boxed{\epsilon_{11} + 2\epsilon_{12} + \epsilon_{22}} / 2$

and so on!!

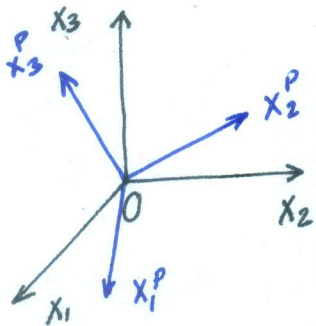
Eigenvalue problem for strain tensor:

$[E]\vec{n} = \lambda \vec{n} \Rightarrow$ we get eigenvalues $\lambda_1, \lambda_2, \lambda_3$
and corresponding eigenvectors $\vec{n}^{(1)}, \vec{n}^{(2)}, \vec{n}^{(3)}$.

- Since $[E]$ is symmetric, $\{\lambda_i\}_{i=1}^3$ is real and

$\vec{n}^{(1)} \perp \vec{n}^{(2)} \perp \vec{n}^{(3)} \Leftarrow$ form an orthogonal coordinate system

principal coordinates / axes. $\rightarrow x_1^p - x_2^p - x_3^p$



Now $[R] = [\vec{n}^{(1)} \ \vec{n}^{(2)} \ \vec{n}^{(3)}]$

$$\Rightarrow [E][R] = [\lambda_1 \vec{n}^{(1)} \ \lambda_2 \vec{n}^{(2)} \ \lambda_3 \vec{n}^{(3)}]$$

$$= [n^{(1)} \ n^{(2)} \ n^{(3)}] \begin{bmatrix} \lambda_1 & 0 & 0 \\ 0 & \lambda_2 & 0 \\ 0 & 0 & \lambda_3 \end{bmatrix}$$

$$\Rightarrow [E][R] = [R][\Lambda] \Rightarrow [E] = [R][\Lambda][R]^T$$

* Note that $\{\Delta x^p\} = [R]^T \{\Delta x\} = [Q] \{\Delta x\}$ with

$$[Q] = [R]^T \Rightarrow [E] = [Q]^T [\Lambda] [Q]$$

or $[\Lambda] = [Q] [E] [Q]^T$

* Note that $\vec{\Delta x}' = \Delta x \vec{n}^{(i)}$ gives $\frac{\Delta l}{l_0} = \lambda_i$

* No shear in principal strain coordinate system.

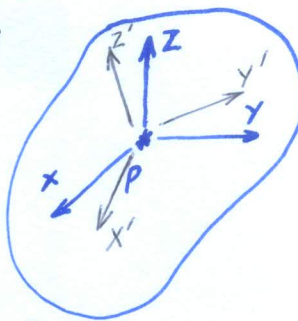
Stress and strain transformation

- Let point P have coordinates (x, y, z)

- Let (x', y', z') be coordinates in a new, rotated coordinate system obtained by:

$$\begin{Bmatrix} x' \\ y' \\ z' \end{Bmatrix} = [R] \begin{Bmatrix} x \\ y \\ z \end{Bmatrix}$$

rotation matrix



Examples of $[R]$:

$$[R] = \begin{bmatrix} \cos \theta_z & \sin \theta_z & 0 \\ -\sin \theta_z & \cos \theta_z & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$[R] = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \theta_x & \sin \theta_x \\ 0 & -\sin \theta_x & \cos \theta_x \end{bmatrix}$$

$$[\sigma'] = [R][\sigma][R]^T \quad ; \quad [e'] = [R][e][R]^T$$

Principal stress directions:

$$[\sigma]\{n\} = \lambda \{n\} \Rightarrow \text{Eigenvalues (principal stresses)} \\ \lambda_1, \lambda_2, \lambda_3$$

Principal directions (or eigenvectors) $\vec{n}^1, \vec{n}^2, \vec{n}^3$ with $|\vec{n}^1| = |\vec{n}^2| = |\vec{n}^3| = 1$
and $\vec{n}^1 \perp \vec{n}^2 \perp \vec{n}^3$.

$$\begin{Bmatrix} \vec{n}^1 \\ \vec{n}^2 \\ \vec{n}^3 \end{Bmatrix} = \begin{bmatrix} n_1^1 & n_2^1 & n_3^1 \\ n_1^2 & n_2^2 & n_3^2 \\ n_1^3 & n_2^3 & n_3^3 \end{bmatrix} \begin{Bmatrix} \hat{i} \\ \hat{j} \\ \hat{k} \end{Bmatrix} \Rightarrow \{\vec{n}\} = \underbrace{[N]}_{[R]^T} \{\hat{i}\} \\ \Rightarrow \boxed{\{x^p\} = [R]^T \{x\}}$$

